

TLR - TLQ

Data sheet - rev. 1.0



LINEAR COMPONENTS

myRollon

myRollon is Rollon's **digital working platform** designed to simplify the selection and configuration of linear and rotary motion solutions. It enables users to identify the most suitable motion system based on their specific application requirements, enhancing design precision and efficiency.

By centralizing essential tools and resources in a unified environment, myRollon empowers users to access all necessary services and information — saving time and boosting productivity in search of high-performance motion solutions.

SCAN ME!



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► FEATURES AND ADVANTAGES



Fig.1

TLR and TLQ are full-extension telescopic rails combining very compact dimensions with high flexural rigidity. The use of a double-row ball bearing system without ball cages reduces sensitivity to high dynamics and variable duty cycles, making them ideal for automated, vertical, or variable-stroke applications, even in the presence of dirt or debris.

TLR rails feature double-row ball bearings and a rigid S-shaped intermediate element, providing high load capacity, low deflection, and smooth, clearance-free motion. A self-aligning version is available for compensating minor misalignments. Size 18 rails are hardened using the Rollon-Nox nitriding and oxidation process, while sizes 28 and 43 feature induction-hardened and fine-ground raceways with multiple anticorrosion treatments available.

TLQ rails adopt a compact square cross-section with double-row ball bearings, offering high axial and radial load capacity with reduced dimensions and weight, particularly advantageous for vertical applications. The stroke/load capacity ratio can be customized by adjusting the distance between the sliders. Size 18 uses the Rollon-Nox nitriding and oxidation process, and sizes 28 and 43 are equipped with induction-hardened, fine-ground raceways with various anticorrosion treatment options.

The TLR and TLQ series are particularly suitable for automation systems, material handling equipment, and industrial and packaging machinery, especially in high-cycle environments requiring robust performance, low maintenance, and stable operation under demanding conditions.

Performance characteristics

- Available sizes: 18, 28, 43
- Max. operating speed: 1 m/s (39 in/s)*
- Temperature range: -20 °C + 110 °C (-4 °F + 230 °F)
- Surface treatments: see Pg.19

* depending on application and stroke

Rails

- Materials: cold drawn carbon steel with induction hardened and ground raceways.
- Available rail lengths: from 290 mm up to 1970 mm (from 11.4 in to 77.6 in)

Rollers

- Materials: Carbon steel 2RS shield and Stainless steel.
- Rollers lubricated for life

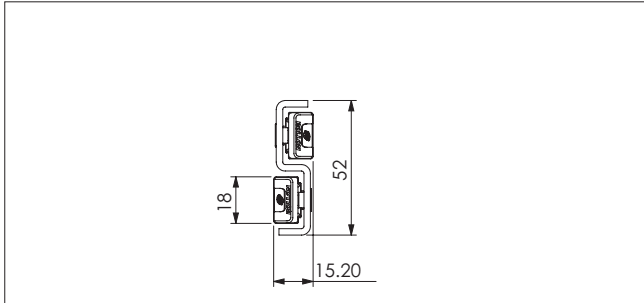
MAIN ADVANTAGES

| Self-aligning system | Reliability | Low deflection | High load capacity | Long service life |
|---|---|---|---|---|
| The TLR self-aligning version compensates for misalignment, reducing assembly time. | The absence of a ball cage enables reliable operation in automated vertical and variable-stroke applications. | Sturdy profiles ensure minimal deflection under load. | Double-row ball bearings and rigid intermediate elements provide elevated axial and radial load capacities. | TLR and TLQ provide wear resistance and contribute to extended operational lifetime, even in high-cycle applications. |

► COMPONENTS AND DIMENSIONS

■ TLR...P-TLQ...P series

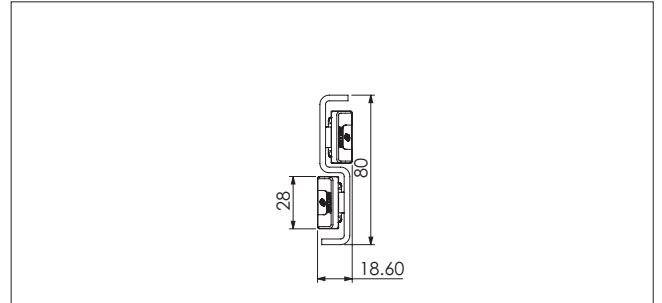
■ TLR18P...R - TLR18P...L



Load capacity Pg.8

Fig.2

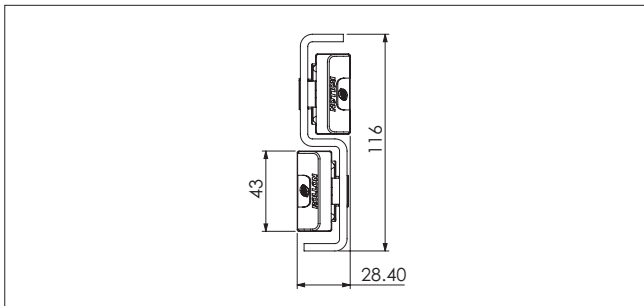
■ TLR28P...R - TLR28P...L



Load capacity Pg.9

Fig.3

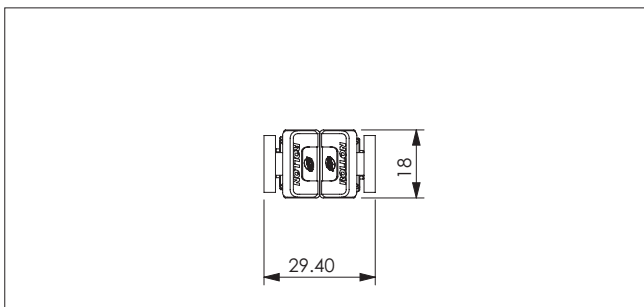
■ TLR43P...R - TLR43P...L



Load capacity Pg.10

Fig.4

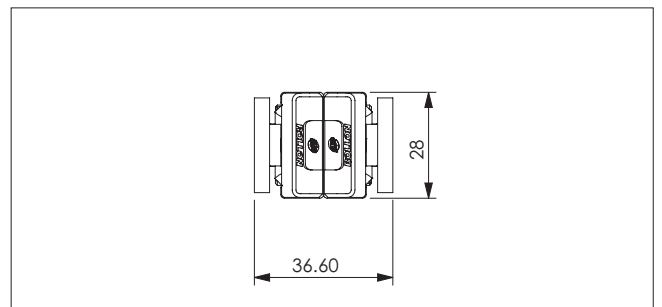
■ TLQ18P



Load capacity Pg.11

Fig.5

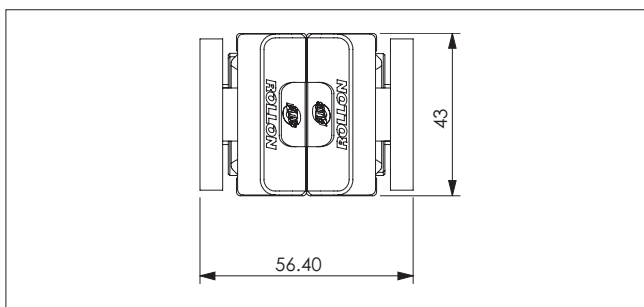
■ TLQ28P



Load capacity Pg.12

Fig.6

■ TLQ43P



Load capacity Pg.13

Fig.7

■ TLR18P

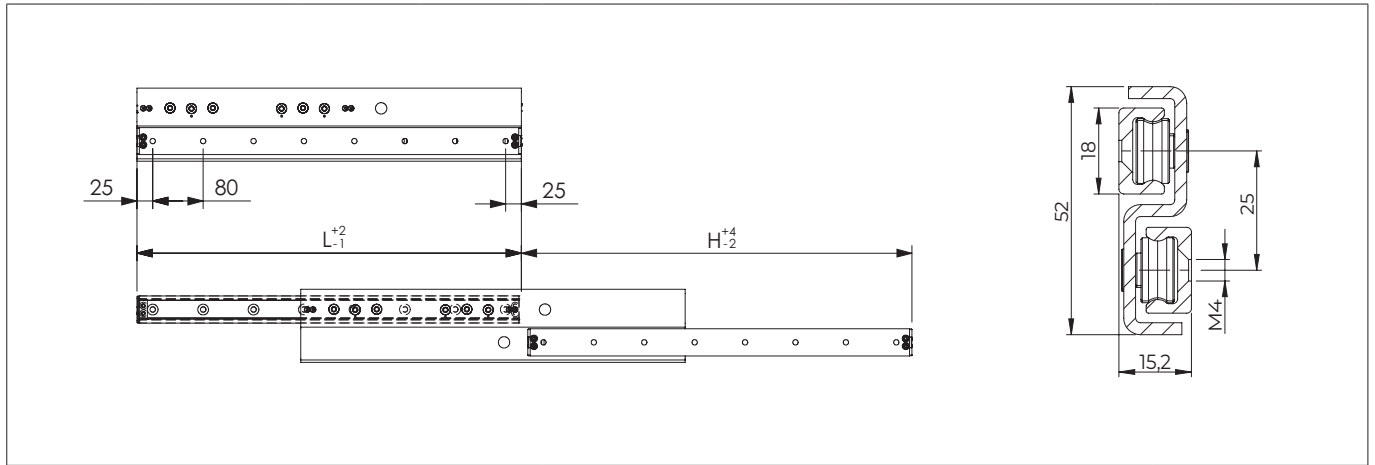
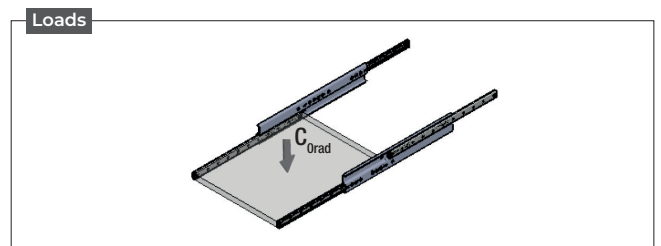


Fig.8

| Type | Size | Length L [mm] | Stroke H [mm] | Load capacity for a pair of rails | | No. of holes | Weight [kg] |
|---------|------|---------------|---------------|-----------------------------------|-----------------------|--------------|-------------|
| | | | | Dynamic load coefficient C* [N] | C _{0rad} [N] | | |
| TLR...P | 18 | 290 | 290 | 1510 | 732 | 4 | 0.9 |
| | | 370 | 370 | 2001 | 970 | 5 | 1.2 |
| | | 450 | 450 | 2291 | 1111 | 6 | 1.4 |
| | | 530 | 530 | 2485 | 1205 | 7 | 1.6 |
| | | 610 | 610 | 2623 | 1272 | 8 | 1.9 |
| | | 690 | 690 | 2727 | 1322 | 9 | 2.1 |
| | | 770 | 770 | 2808 | 1361 | 10 | 2.3 |

Tab.1

*Only for lifetime calculation, see pg.22
 Rails in left and right version when used in pair:
 TLR18P...L left version
 TLR18P...R right version



■ TLR28P

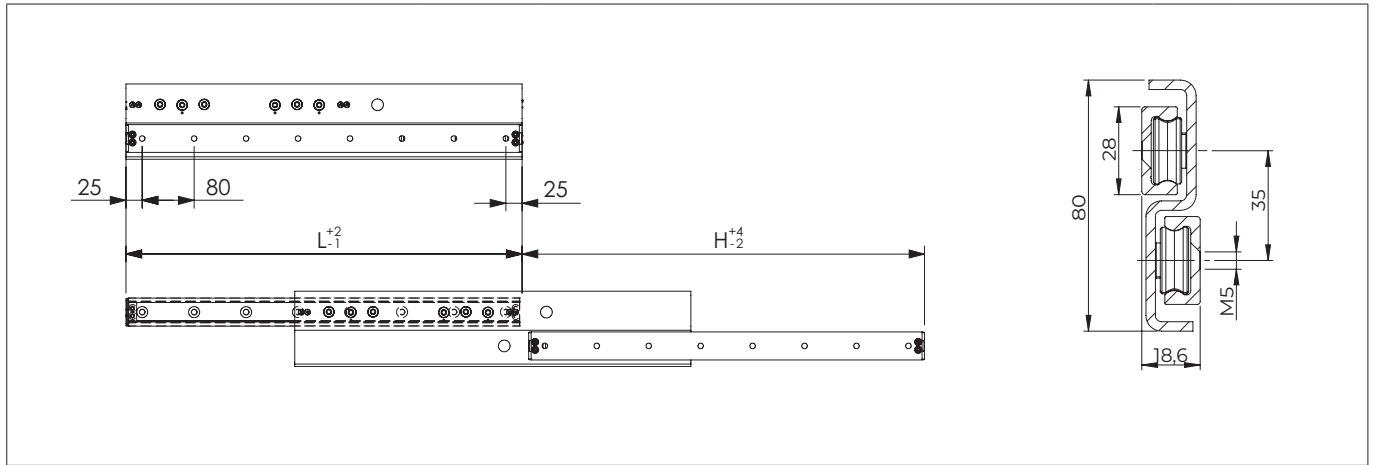
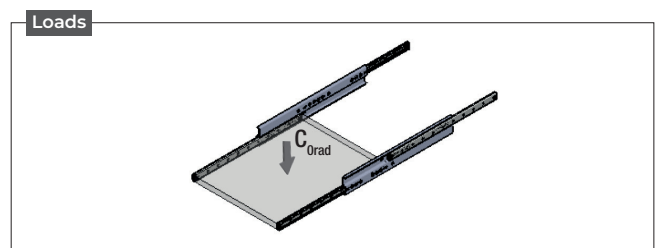


Fig.9

| Type | Size | Length L [mm] | Stroke H [mm] | Load capacity for a pair of rails | | No. of holes | Weight [kg] |
|---------|------|---------------|---------------|-----------------------------------|-----------------------|--------------|-------------|
| | | | | Dynamic load coefficient C* [N] | C _{Orad} [N] | | |
| TLR...P | 28 | 370 | 380 | 2362 | 1275 | 5 | 2.1 |
| | | 450 | 460 | 3401 | 1835 | 6 | 2.5 |
| | | 530 | 540 | 3893 | 2101 | 7 | 2.9 |
| | | 610 | 620 | 5490 | 2963 | 8 | 3.3 |
| | | 690 | 700 | 5981 | 3227 | 9 | 3.7 |
| | | 770 | 780 | 6215 | 3354 | 10 | 4.1 |
| | | 850 | 860 | 6403 | 3455 | 11 | 4.5 |
| | | 930 | 940 | 6556 | 3267 | 12 | 4.9 |
| | | 1010 | 1020 | 6684 | 3041 | 13 | 5.3 |
| | | 1090 | 1100 | 6792 | 2844 | 14 | 5.7 |
| | | 1170 | 1180 | 6885 | 2672 | 15 | 6.1 |
| | | 1250 | 1260 | 6965 | 2519 | 16 | 6.5 |
| | | 1330 | 1340 | 7035 | 2382 | 17 | 6.9 |
| | | 1410 | 1420 | 7097 | 2260 | 18 | 7.3 |
| 1490 | 1500 | 7152 | 2149 | 19 | 7.7 | | |

Tab.2

*Only for lifetime calculation, see pg.22
 Rails in left and right version when used in pair:
 TLR28P...L left version
 TLR28P...R right version



■ TLR43P

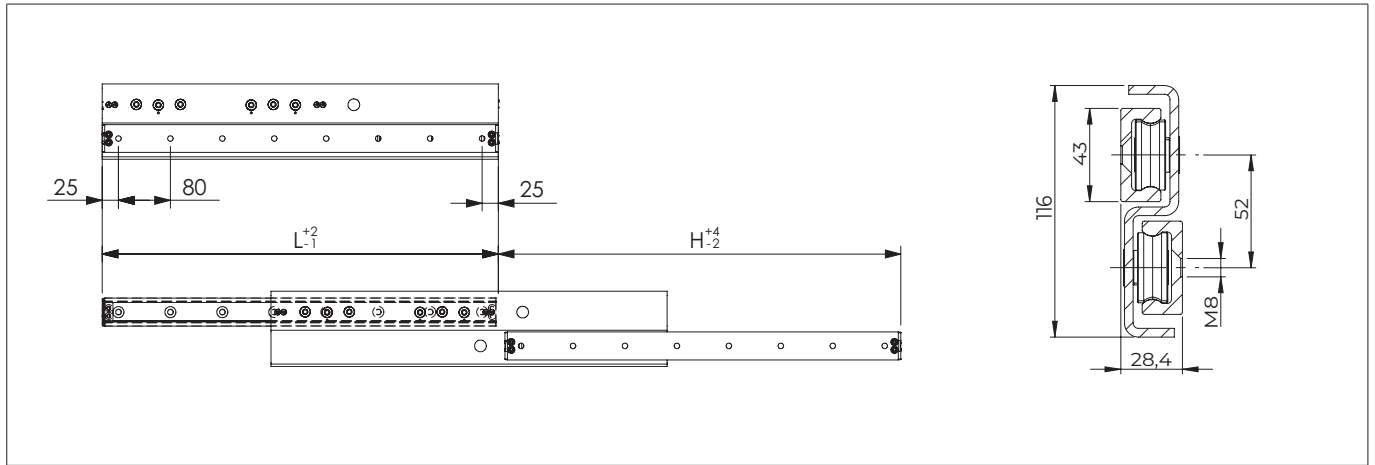
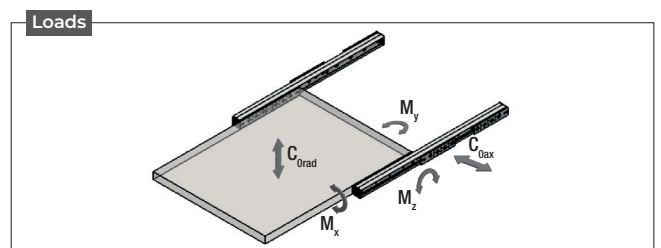


Fig.10

| Type | Size | Length L [mm] | Stroke H [mm] | Load capacity for a pair of rails | | No. of holes | Weight [kg] |
|---------|------|---------------|---------------|-----------------------------------|-----------------------|--------------|-------------|
| | | | | Dynamic load coefficient C* [N] | C _{Orad} [N] | | |
| TLR...P | 43 | 530 | 540 | 3891 | 2205 | 7 | 6.4 |
| | | 610 | 620 | 7501 | 4251 | 8 | 7.3 |
| | | 690 | 700 | 9725 | 4805 | 9 | 8.2 |
| | | 770 | 780 | 10497 | 5949 | 10 | 9.1 |
| | | 850 | 860 | 13428 | 7256 | 11 | 10.0 |
| | | 930 | 940 | 14266 | 8085 | 12 | 10.9 |
| | | 1010 | 1020 | 14691 | 8326 | 13 | 11.8 |
| | | 1090 | 1100 | 15050 | 8040 | 14 | 12.7 |
| | | 1170 | 1180 | 15356 | 7568 | 15 | 13.6 |
| | | 1250 | 1260 | 15621 | 7148 | 16 | 14.5 |
| | | 1330 | 1340 | 15852 | 6773 | 17 | 15.4 |
| | | 1410 | 1420 | 16055 | 6435 | 18 | 16.3 |
| | | 1490 | 1500 | 16235 | 6129 | 19 | 17.2 |
| | | 1570 | 1580 | 16397 | 5851 | 20 | 18.1 |
| | | 1650 | 1660 | 16541 | 5597 | 21 | 19.0 |
| | | 1730 | 1740 | 16672 | 5364 | 22 | 19.9 |
| | | 1810 | 1820 | 16791 | 5150 | 23 | 20.8 |
| | | 1890 | 1900 | 16899 | 4952 | 24 | 21.7 |
| 1970 | 1980 | 16998 | 4769 | 25 | 22.6 | | |

Tab.3

*Only for lifetime calculation, see pg.22
 Rails in left and right version when used in pair:
 TLR43P...L left version
 TLR43P...R right version



■ TLQ18P

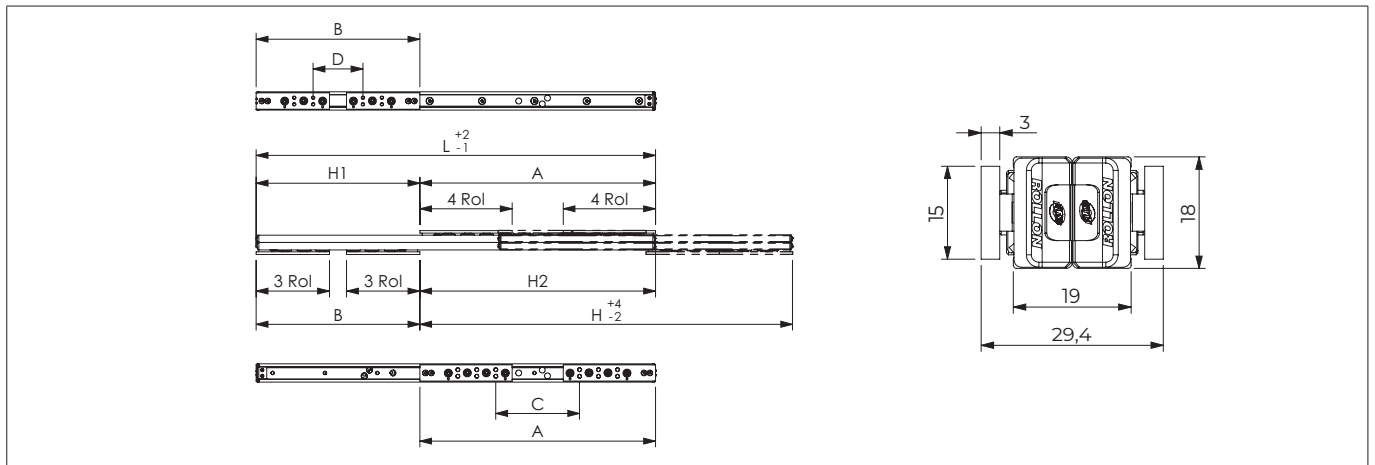


Fig.11

| Type | Size | L [mm] | H [mm] | Fixed sliders*3 | | | Mobile sliders*2 | | | Load capacity and moments for a pair of rails | | | | | |
|---------|------|--------|--------|-----------------|--------|---------|------------------|--------|---------|---|-----------------------|----------------------|------------------------|---------------------|---------------------|
| | | | | A [mm] | C [mm] | H1 [mm] | B [mm] | D [mm] | H2 [mm] | Dynamic load coefficient C**4 [N] | C _{grad} [N] | C _{oax} [N] | M _x *1 [Nm] | M _y [Nm] | M _z [Nm] |
| TLQ...P | 18 | 370 | 370 | 185 | 47 | 185 | 185 | 47 | 185 | 1009 | 447 | 282 | 6 | 88 | 110 |
| | | 450 | 450 | 270 | 132 | 180 | 180 | 42 | 270 | 1619 | 863 | 379 | 6 | 81 | 102 |
| | | 530 | 530 | 318 | 180 | 212 | 212 | 74 | 318 | 1770 | 771 | 332 | 6 | 107 | 153 |
| | | 610 | 610 | 366 | 228 | 244 | 244 | 106 | 366 | 1878 | 687 | 296 | 6 | 107 | 204 |
| | | 690 | 690 | 414 | 276 | 276 | 276 | 138 | 414 | 1959 | 618 | 266 | 6 | 107 | 250 |
| | | 770 | 770 | 462 | 324 | 308 | 308 | 170 | 462 | 2021 | 563 | 242 | 6 | 107 | 250 |

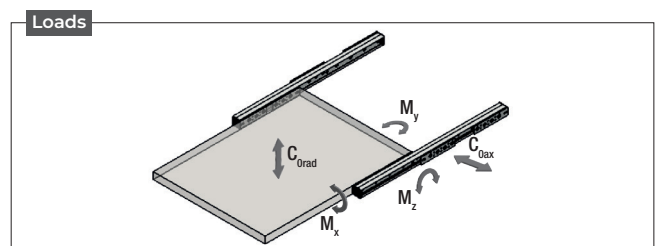
Tab.4

*1 The value M_x refers to a single rail

*2 All mobile sliders are of the three-roller type

*3 For size 18 all fixed sliders are 3 rollers type

*4 Only for lifetime calculation, see pg.22



■ TLQ28P

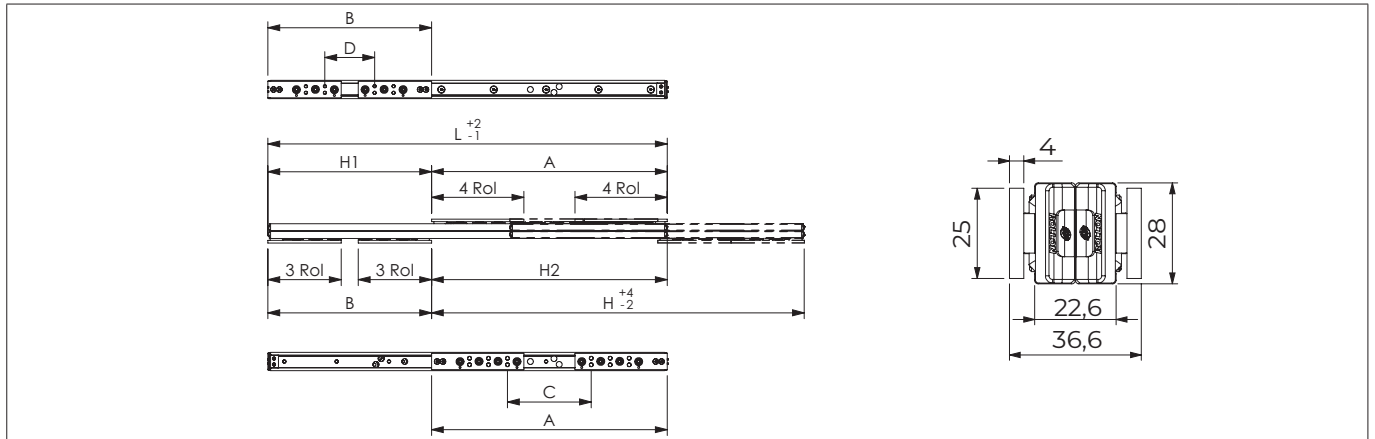


Fig.12

| Type | Size | L [mm] | H [mm] | Fixed sliders ^{*3} | | | Mobile sliders ^{*2} | | | Load capacity and moments for a pair of rails | | | | | |
|---------|------|--------|--------|-----------------------------|--------|---------|------------------------------|--------|---------|---|-----------------------|----------------------|-----------------------------------|---------------------|---------------------|
| | | | | A [mm] | C [mm] | H1 [mm] | B [mm] | D [mm] | H2 [mm] | Dynamic load coefficient C ^{*4} [N] | C _{Orad} [N] | C _{Oax} [N] | M _x ^{*1} [Nm] | M _y [Nm] | M _z [Nm] |
| TLQ...P | 28 | 450 | 450 | 227 | 53 | 223 | 223 | 49 | 227 | 1130 | 871 | 514 | 18 | 190 | 253 |
| | | 530 | 530 | 307 | 133 | 223 | 223 | 49 | 307 | 1980 | 1527 | 775 | 18 | 190 | 253 |
| | | 610 | 610 | 360 | 128 | 250 | 250 | 76 | 360 | 2672 | 2060 | 790 | 18 | 252 | 336 |
| | | 690 | 690 | 408 | 176 | 282 | 282 | 108 | 408 | 2917 | 1875 | 717 | 18 | 310 | 438 |
| | | 770 | 770 | 456 | 224 | 314 | 314 | 140 | 456 | 3105 | 1716 | 656 | 18 | 310 | 541 |
| | | 850 | 850 | 504 | 272 | 346 | 346 | 172 | 504 | 3254 | 1582 | 605 | 18 | 310 | 643 |
| | | 930 | 930 | 552 | 320 | 378 | 378 | 204 | 552 | 3374 | 1467 | 561 | 18 | 310 | 746 |
| | | 1010 | 1010 | 600 | 368 | 410 | 410 | 236 | 600 | 3474 | 1368 | 523 | 18 | 310 | 810 |
| | | 1090 | 1090 | 648 | 416 | 442 | 442 | 268 | 648 | 3558 | 1282 | 490 | 18 | 310 | 810 |
| | | 1170 | 1170 | 696 | 464 | 474 | 474 | 300 | 696 | 3630 | 1205 | 461 | 18 | 310 | 810 |
| | | 1250 | 1250 | 744 | 512 | 506 | 506 | 332 | 744 | 3691 | 1138 | 435 | 18 | 310 | 810 |
| | | 1330 | 1330 | 792 | 560 | 538 | 538 | 364 | 792 | 3745 | 1077 | 412 | 18 | 310 | 810 |
| 1410 | 1410 | 840 | 608 | 570 | 570 | 396 | 840 | 3792 | 1023 | 391 | 18 | 310 | 810 | | |
| 1490 | 1490 | 888 | 656 | 602 | 602 | 428 | 888 | 3834 | 974 | 372 | 18 | 310 | 810 | | |

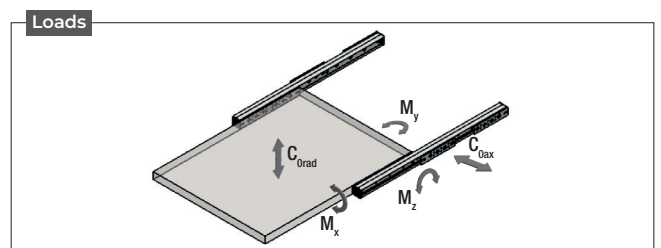
Tab.5

*1 The value Mx refers to a single rail

*2 All mobile sliders are of the three-roller type

*3 For size 28, fixed sliders with lengths of 450-530 mm are of the three-roller type; longer lengths are of the four-roller type

*4 Only for lifetime calculation, see pg.22



■ TLQ43P

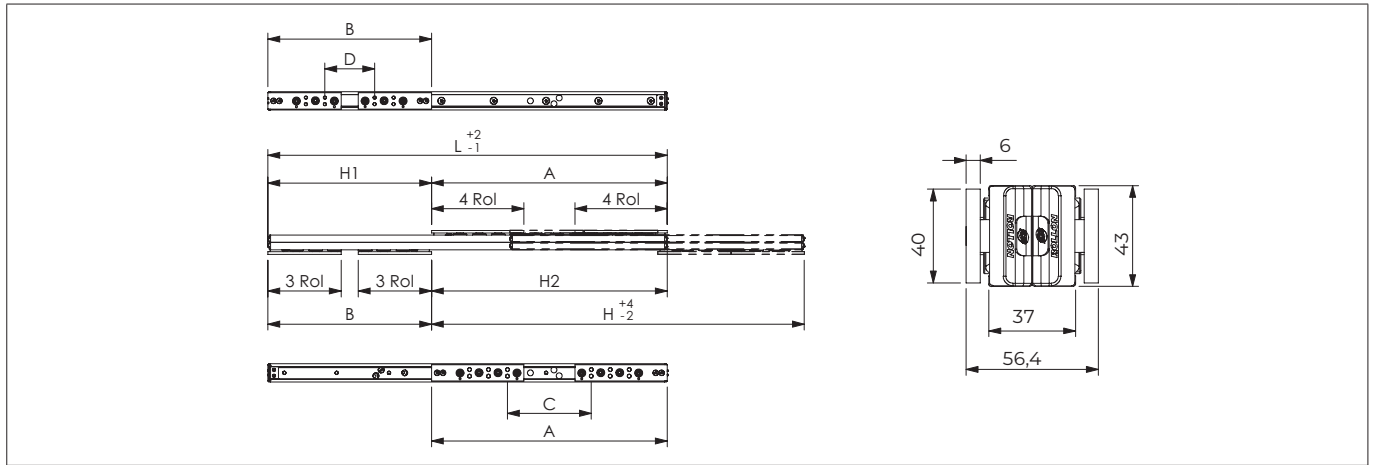


Fig.13

| Type | Size | L [mm] | H [mm] | Fixed sliders ^{*3} | | | Mobile sliders ^{*2} | | | Load capacity and moments for a pair of rails | | | | | |
|---------|------|--------|--------|-----------------------------|--------|---------|------------------------------|--------|---------|---|-----------------------|----------------------|-----------------------------------|---------------------|---------------------|
| | | | | A [mm] | C [mm] | H1 [mm] | B [mm] | D [mm] | H2 [mm] | Dynamic load coefficient C ^{*4} [N] | C _{0rad} [N] | C _{0ax} [N] | M _x ^{*1} [Nm] | M _y [Nm] | M _z [Nm] |
| TLQ...P | 43 | 610 | 600 | 310 | 78 | 300 | 310 | 78 | 300 | 2841 | 2300 | 1829 | 64 | 690 | 920 |
| | | 690 | 690 | 374 | 142 | 316 | 316 | 84 | 374 | 4132 | 3345 | 2359 | 64 | 1044 | 1008 |
| | | 770 | 770 | 456 | 140 | 314 | 314 | 82 | 456 | 6218 | 5034 | 2084 | 64 | 1044 | 944 |
| | | 850 | 850 | 504 | 188 | 346 | 346 | 114 | 504 | 6708 | 5357 | 1930 | 64 | 1044 | 1200 |
| | | 930 | 930 | 552 | 236 | 378 | 378 | 146 | 552 | 7103 | 4988 | 1797 | 64 | 1044 | 1456 |
| | | 1010 | 1010 | 600 | 284 | 410 | 410 | 178 | 600 | 7428 | 4667 | 1681 | 64 | 1044 | 1712 |
| | | 1090 | 1090 | 648 | 332 | 442 | 442 | 210 | 648 | 7701 | 4384 | 1579 | 64 | 1044 | 1968 |
| | | 1170 | 1170 | 696 | 380 | 474 | 474 | 242 | 696 | 7932 | 4134 | 1489 | 64 | 1044 | 2224 |
| | | 1250 | 1250 | 744 | 428 | 506 | 506 | 274 | 744 | 8131 | 3911 | 1409 | 64 | 1044 | 2480 |
| | | 1330 | 1330 | 792 | 476 | 538 | 538 | 306 | 792 | 8304 | 3711 | 1337 | 64 | 1044 | 2736 |
| | | 1410 | 1410 | 840 | 524 | 570 | 570 | 338 | 840 | 8456 | 3530 | 1272 | 64 | 1044 | 2898 |
| | | 1490 | 1490 | 888 | 572 | 602 | 602 | 370 | 888 | 8590 | 3366 | 1213 | 64 | 1044 | 2898 |
| | | 1570 | 1570 | 936 | 620 | 634 | 634 | 402 | 936 | 8710 | 3216 | 1159 | 64 | 1044 | 2898 |
| | | 1650 | 1650 | 984 | 668 | 666 | 666 | 434 | 984 | 8817 | 3080 | 1109 | 64 | 1044 | 2898 |
| | | 1730 | 1730 | 1032 | 716 | 698 | 698 | 466 | 1032 | 8914 | 2954 | 1064 | 64 | 1044 | 2898 |
| | | 1810 | 1810 | 1080 | 764 | 730 | 730 | 498 | 1080 | 9001 | 2838 | 1023 | 64 | 1044 | 2898 |
| 1890 | 1890 | 1128 | 812 | 762 | 762 | 530 | 1128 | 9081 | 2731 | 984 | 64 | 1044 | 2898 | | |
| 1970 | 1970 | 1176 | 860 | 794 | 794 | 562 | 1176 | 9154 | 2632 | 948 | 64 | 1044 | 2898 | | |

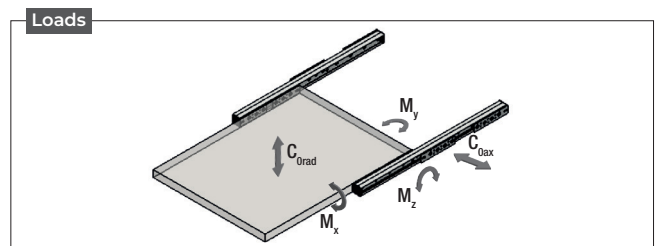
Tab.6

*1 The value M_x refers to a single rail

*2 All mobile sliders are of the three-roller type

*3 For lengths 610-690mm fixed sliders are of the three-roller type; longer lengths are of the four-roller type

*4 Only for lifetime calculation, see pg.22



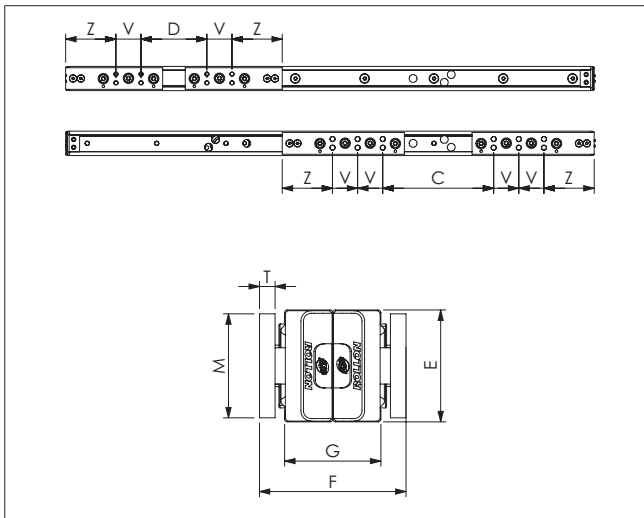
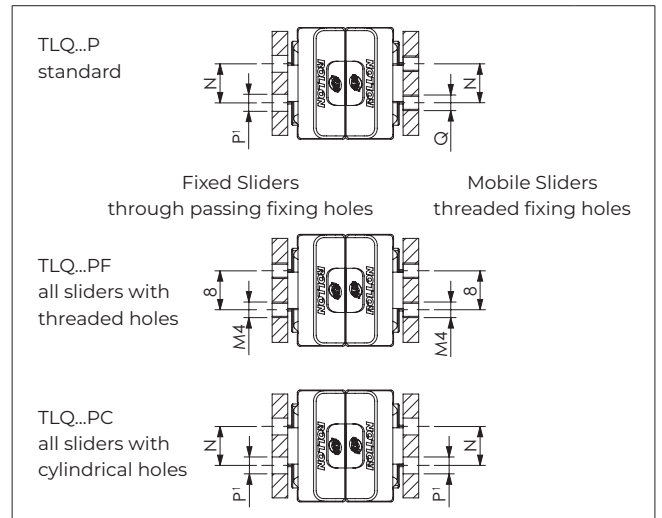


Fig.14



¹ Fixing holes (P) for fixing screw according to DIN 912.

Fig.15

| Type | Size | E [mm] | F [mm] | G [mm] | M [mm] | T [mm] | N [mm] | P [mm] | Q | Sliders | | Z [mm] | V [mm] | Weight [kg/m] | Weight 4 sliders [Kg] |
|---------|------|--------|--------|--------|--------|--------|--------|--------|----|-----------------|-------------|--------|--------|---------------|-----------------------|
| | | | | | | | | | | Num. of rollers | Length [mm] | | | | |
| TLQ...P | 18 | 18 | 29.4 | 19 | 15 | 3 | 8 | - | M4 | 3 | 87 | 48 | 21 | 1.4 | 0.4 |
| | 28 | 28 | 36.6 | 22.6 | 25 | 4 | 10 | Ø5.5 | M5 | 3 | 112 | 58 | 29 | 2.5 | 1.5 |
| | | | | | | | | | | 4 | 141 | | | | |
| 43 | 43 | 56.4 | 37 | 40 | 6 | 15 | Ø6.5 | M6 | 3 | 155 | 74 | 42 | 6 | 2.4 | |
| | | | | | | | | | 4 | 197 | | | | | |

Tab.7

Three options for fixing holes available (see fig.15). Rail size 18 is only available in F version with all threaded holes. When used in pairs, the same rail can be installed left or right just by rotating it. See "Installation Instructions" on pg.20.

▶ ACCESSORIES

■ Fixing screws

TLR...P

We recommend countersunk head screws according to DIN 7991

| Type | Size | V |
|---------|------|----|
| TLR...P | 18 | M4 |
| | 28 | M5 |
| | 43 | M8 |

Tab.8

TLQ...P

We recommend fixing screws according to DIN 912 for the fixed sliders in TLQ...P and fixed and mobile sliders in TLQ...PC.

| Type | Size | V |
|---------|------|----|
| TLQ...P | 18 | M4 |
| | 28 | M5 |
| | 43 | M8 |

Tab.9

▶ USE AND MAINTENANCE

■ Telescopic rail selection

Selecting the suitable telescopic rail should be done based on the load and the maximum permissible deflection in the extended state. The load capacity of a Telerace telescopic rail depends on two factors: the load capacity of the rollers and the rigidity of the intermediate element. For mainly short strokes, the load capacity is determined by the load-bearing capacity of the rollers; for average and long strokes, it is determined by the rigidity of the intermediate element.

■ Deflection

If the load P acts vertically on the pair of rails (see Fig.17), the expected elastic deflection in the extended state can be determined as follows:

$$f = \frac{q}{t} \cdot P$$

Fig.16

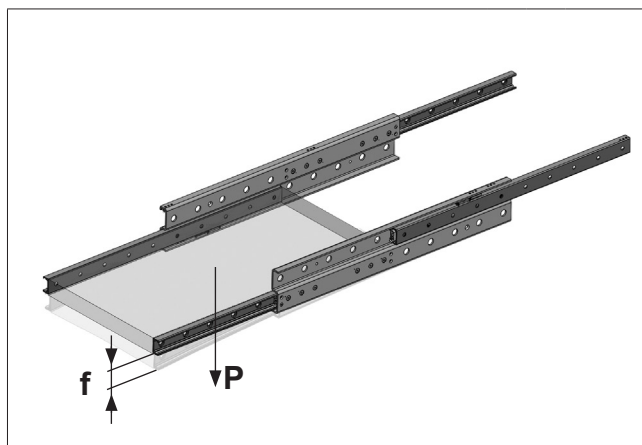


Fig.17

Whereby:

f is the expected elastic deflection [mm]

q is a stroke coefficient (see Fig.19)

t is a factor depending on the model of the telescopic rail (see Fig.18)

P is the actual load acting on the center of a pair of rails [N].

The value resulting from the formula above is an estimation and also assumes an absolutely rigid adjacent construction. If this rigidity is not present, or in case the deflection is a key application requirement, please contact our technical department for a precise calculation.

| | |
|---------------|---------------|
| TLR18P t=300 | TLQ18P t= 60 |
| TLR28P t=500 | TLQ28P t=120 |
| TLR43P t=1200 | TLQ43P t= 450 |

Fig.18

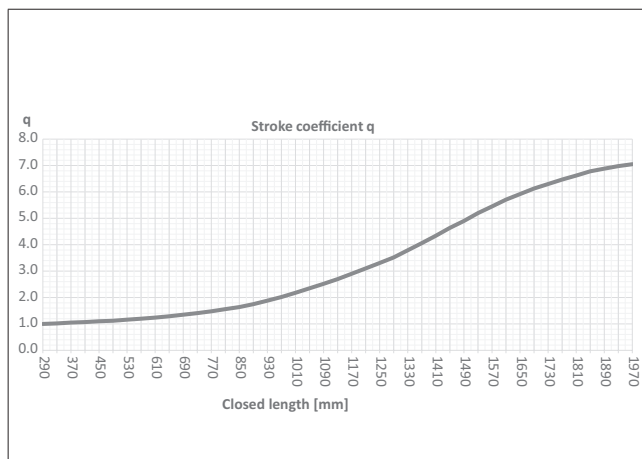


Fig.19

■ Opening and closing force

For applications requiring very low opening and closing forces, the rails series TLR...P and TLQ...P are recommended. The required force F_e to extend a pair of rails is determined by the friction of the rolling elements and the applied load P , according to the following formula:

$$F_e \approx k + 0.01 \cdot P$$

Fig.20

The required force F_c to close a pair of rails is also influenced by the deflection and the stroke, according to the the following formula:

$$F_c \approx k + 0.01 \cdot P + 1.5 \cdot \frac{f}{H} \cdot P$$

Fig.21

Where :

P = radial load applied on the pair of rails

f = calculated deflection

H = stroke

k = friction force per pair of telescopic rails connected without load applied

| | |
|-----------------|--------|
| TLR18P / TLQ18P | k=10 N |
| TLR28P / TLQ28P | k=15 N |
| TLR43P / TLQ43P | k=25 N |

Fig.22

These calculated values may be influenced by some additional binding friction from non-precise assembly or structure. For a single rail, the same formulas can be used.

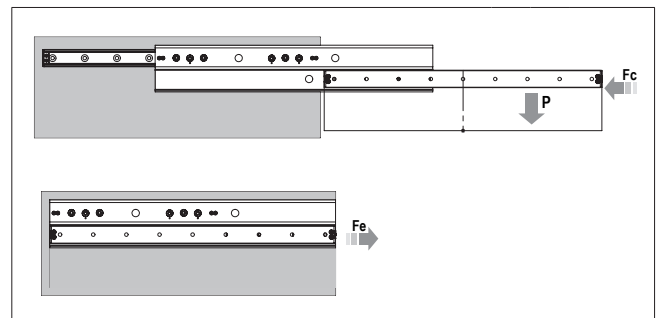


Fig.23

■ Lubrication

TLR...P and TLQ...P rails are equipped with internal wipers with slow release felts that ensure a proper lubrication of the raceways for all the product's lifetime if the rail is used in indoor, clean, environments. The rollers are also lubricated for life. If used in harsh environments (eg. dirt, temperature, humidity) it is necessary to periodically clean and lubricate the raceways.

■ Anticorrosion treatments

TLQ...P

| Treatment | Characteristics |
|-------------------------|---|
| Rollon-Nox | Patented high depth nitride hardening and black oxidation treatment that provides good durability under high loads or frequencies. It is standard for size 18 and it's not available for other sizes. |
| Zinc Plating ISO 2081 | Standard treatment for rails sizes 28-43, it is ideal for indoor applications. It is removed from the raceways by the subsequent grinding process. Zinc-plated telescopic rails are supplied with steel rollers. |
| ZincNickel ISO19598 (Z) | Ideal for outdoor applications. Telescopic rails with this treatment are supplied with stainless steel rollers to further increase the corrosion resistance. |
| Rollon E-coating (K) | Electro painting that provides a fine black finishing to the entire rail. It can be partially removed from the raceways on the running contact point of the rollers after a period of use. Telescopic rails with Rollon E-Coating are supplied with stainless steel rollers to further increase the corrosion resistance. |
| Nickel Plating (N) | Provides high resistance to chemical corrosion and is ideal for applications in medical or food related environments. Raceways are coated too. Telescopic rails with Nickel Plating treatment are supplied with stainless steel rollers to further increase the corrosion resistance. |

Tab.10

■ Speed

The speed of the rails is limited by the strength of the stoppers that take on the intermediate element with each opening/closing. At the same speed, the impact force increases proportionally to the length of the rail and the weight of the intermediate element.

All Telerace telescopic rails feature robust end-stoppers capable of sustaining high speeds. Besides highest speed, the telescopic rails with ball bearing rollers are also less sensitive to frequent and intense accelerations and decelerations due to absence of the ball cage.

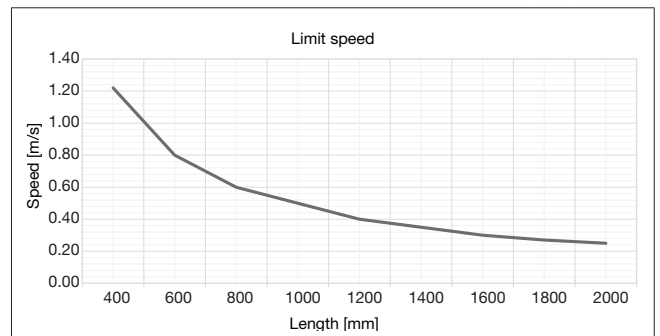


Fig.24

■ Self-aligning system with TLR...AP

TLR...P telescopic rails are also available in the TLR...AP version that allows a slight rotation of the movable element around the longitudinal axis, with respect to the fixed element. This rotation is obtained by using a combination of floating and guiding rollers and allows the rail to adapt to mounting surfaces that are not perfectly aligned in their frontal part, avoiding the overload of the rollers and the deterioration of the motion quality. This same rotation also permits a slight compensation of an eventual dimensional gap between the fixed and mobile structures, that may occur due to manufacturing tolerances, with respect to the nominal dimensions of the rail.

The compensating rail TLR...AP must be used as a pair with a guiding rail TLR...P to ensure the perfect operation of the system and an optimal lateral stability.

Below are listed 3 examples of compensation of structural errors: A) Maximum angular compensation (α_1) of misaligned mounting surfaces of the mobile structure.

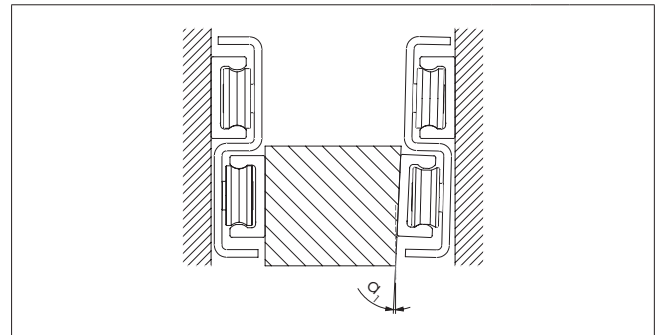


Fig.25

B) Maximum angular compensation (α_2) of misaligned mounting surfaces of the fixed structure

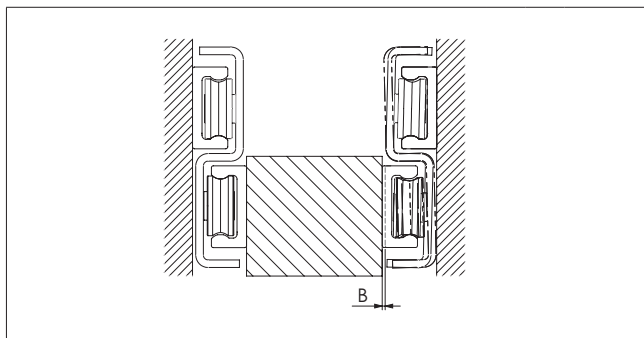


Fig.26

C) Maximum linear compensation (B) of the dimensional gap between mobile and fixed structure for a rail with parallel mounting surfaces.

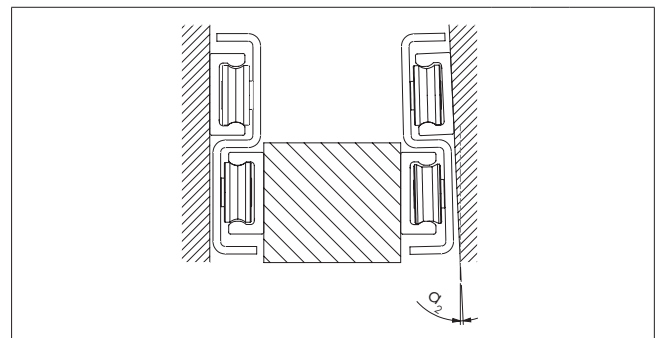


Fig.27

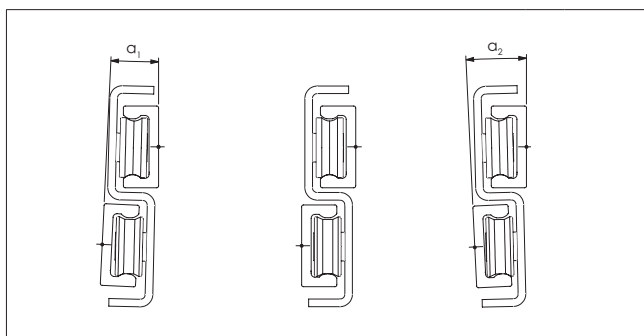


Fig.28

| Size | α_1 [°] | α_2 [°] | B [mm] |
|------|----------------|----------------|--------|
| 18 | 1 | 1 | 0.3 |
| 28 | 0.85 | 0.85 | 0.3 |
| 43 | 1.3 | 1.3 | 0.5 |

Tab.11

■ Stroke customization for TLQ...P

TLQ...P series offer the unique possibility to easily customize the actual stroke H to individual needs. This is obtained by repositioning the slider distance "A" for "Fixed sliders" and distance "B" for "Mobile sliders", with different distances than standard. Please consider that distance A should always be longer than distance B to maximize the load capacity. If the distance between fixed sliders "A" and mobile sliders "B" is reduced, the total stroke increases and the load capacity decreases. Vice versa, the total stroke decreases and the load capacity is improved. Please contact our technical department for load capacities according to customized stroke.

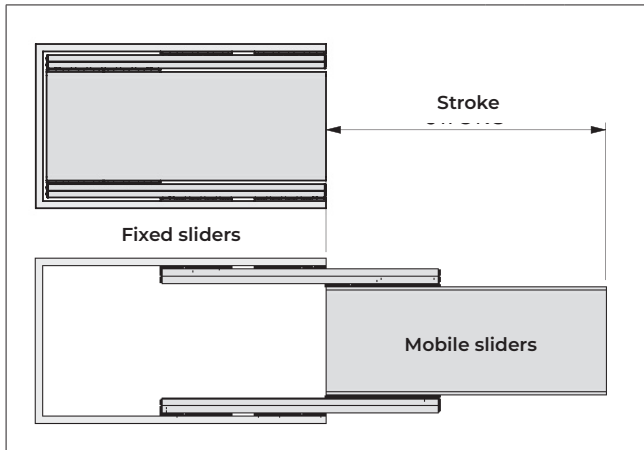


Fig.29

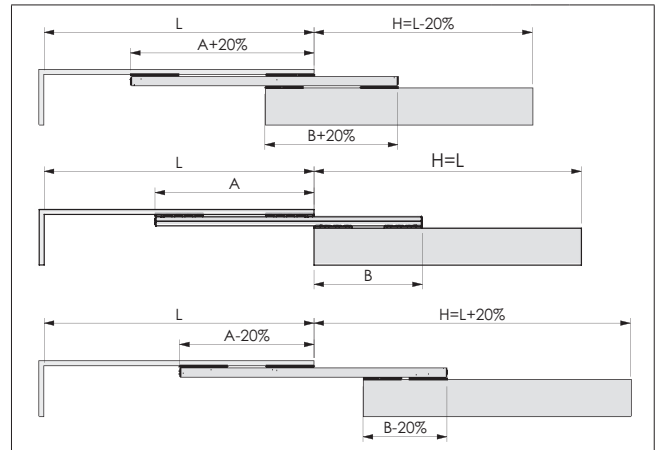
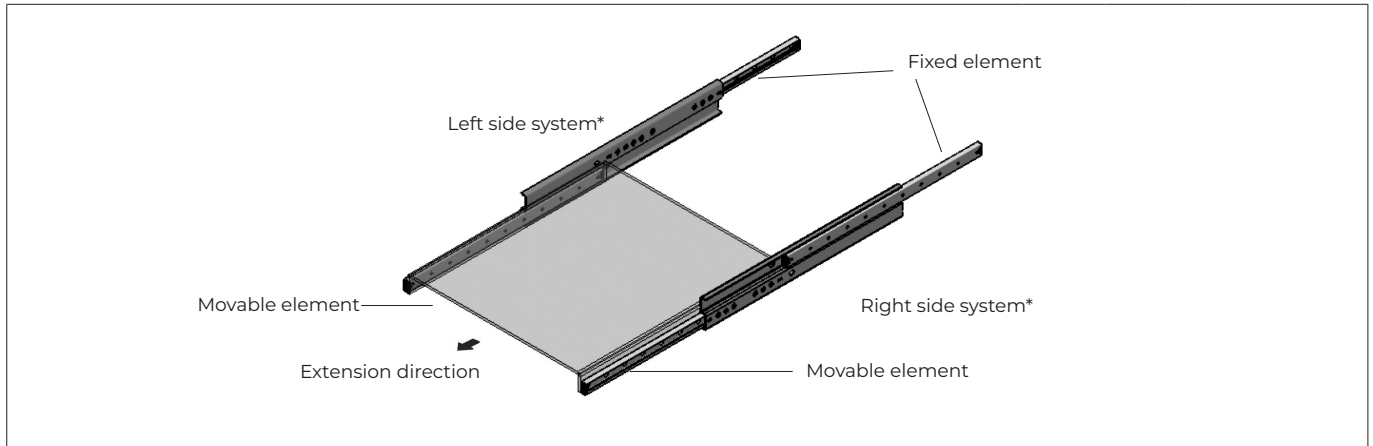


Fig.30

■ Installation instructions

In general and for specific product series



* For model TLR...P please observe right or left side use.

Fig.31

General

- To achieve optimum running properties, high service life and rigidity, it is necessary to fix the telescopic rails with all accessible holes on a rigid and level surface.
- Please observe the parallelism of the installation surfaces. The fixed and movable rails must be fit to a rigid assembly construction.
- Telerace rails are suitable for continuous use in automatic systems, even when the stroke is not constant. The operating speed must be checked (see Pg.17).

TLR...P

- This series accepts radial loads. This should act in the vertical cross-sectional axis on the movable rails.
- Horizontal and vertical application is possible. Prior to vertical installation, please contact our technical department.
- When installing, make sure that the load is placed on the movable element (the lower rail) (see fig. 31). The opposite assembly negatively affects the function.
- Installation must be done on a rigid structure using all accessible fixing holes.
- Pay attention to the parallel alignment during assembly with paired application. It is possible to compensate minor misalignment errors by pairing TLR...P with TLR...AP (see Pg.18)

TLQ...P

- This series accepts radial and axial loads and moments in all principal directions.
- Horizontal and vertical applications are possible. Prior to vertical installation, please contact our technical department.
- The rail must be installed with the label facing upward. The fixed sliders have the circular engraving mark facing upward, while on the mobile sliders the same mark is facing downward.
- When used in pairs, the same rail can be used as left or right rail, always keeping the mark facing upwards.

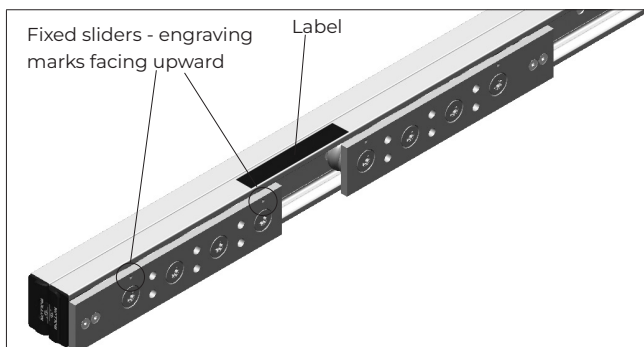


Fig.32

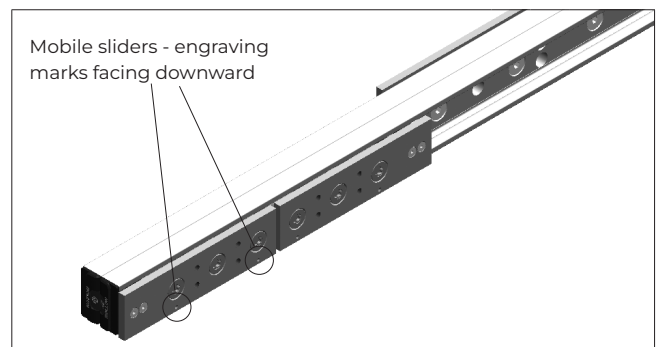


Fig.33

▶ STATIC LOAD AND SERVICE LIFE

■ Sizing of telescopic applications

Selecting the suitable telescopic rail should be done based on the load and the maximum permissible deflection in the extended state. The load capacity of a Telerace telescopic rail depends on two factors: the load capacity of the rollers and the rigidity of the intermediate element. For mainly short strokes the load capacity is determined by the load-bearing capacity of the rollers; for average and long strokes it is determined by the rigidity of the intermediate element.

The main factors to consider while sizing the rail for a telescopic movement are:

- Weight of the mobile part and other applicable loads
- Presence of dynamic forces / eventual abuse
- Max. acceptable deflection
- Max. acceptable extraction/closing force of mobile part
- Environment, frequency and speed
- Expected lifetime

All load capacities C_{0rad} are indicated per pair of rails and with the load perfectly centered. Hereby the load P is acting as a radial point load, at half the extension and in the middle between the two rails. The load capacity for a single rail is obtained dividing the value C_{0rad} by half.

When sizing a telescopic application, consider the center of mass of the load and any external dynamic forces acting on the rails.

In case the actual load P isn't centered the equivalent load P_e must be calculated for the verification of load capacity explained on Pg.14.

$$P_e = 2 \cdot \frac{P \cdot d}{a + b}$$

Fig.34

Where :

P = Weight/load of mobile part [N]

a, b = distances of the load center with respect to left and right rail [mm].

d = the largest between "a" and "b", according to the load position [N].

If the load is not positioned halfway on the mobile slider but with a deviation c from its center, contact the technical department.

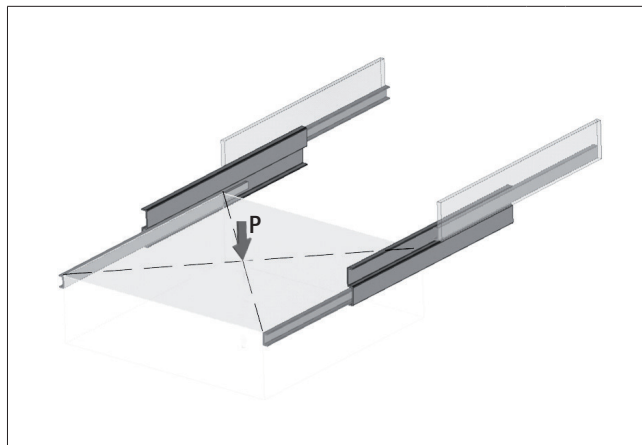


Fig.35

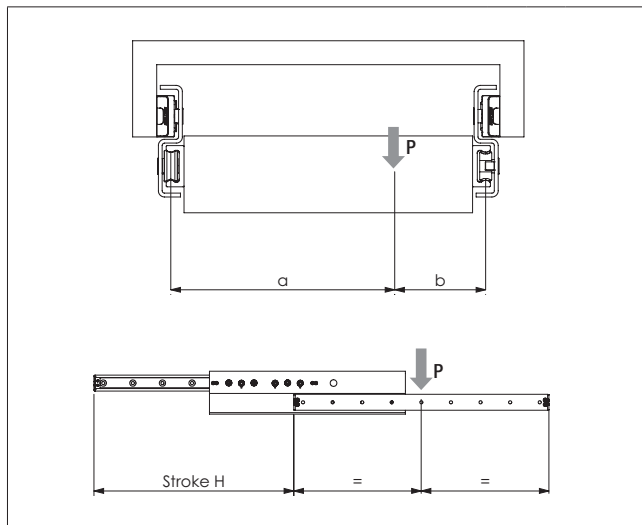


Fig.36

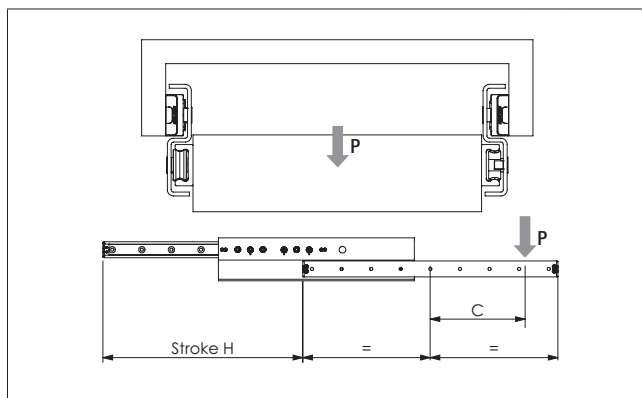


Fig.37

■ **Verification of load capacity**

Verification of the load capacity assumes the knowledge of the forces acting on the rails in the different directions, divided into principal components correspondent to the values indicated in the tables of the product pages: radial loads, axial loads and moments.

For the telescopic rails TLR...P, the verification is mainly down to comparing the load capacity C_{Orad} to Pe , including a safety factor S_0 .

$$Pe \leq C_{Orad} / S_0$$

Fig.38

Where S_0 is the safety coefficient as per below table

| Safety coefficient - S_0 | Application conditions |
|----------------------------|--|
| 1 - 1.5 | Neither shocks nor vibrations, smooth and low-frequency reverse, high assembly accuracy, no elastic deformations |
| 1.5 - 2 | Normal installation conditions |
| 2 - 3.5 | Shocks and vibrations, high-frequency reverse, significant elastic deformation |

Tab.12

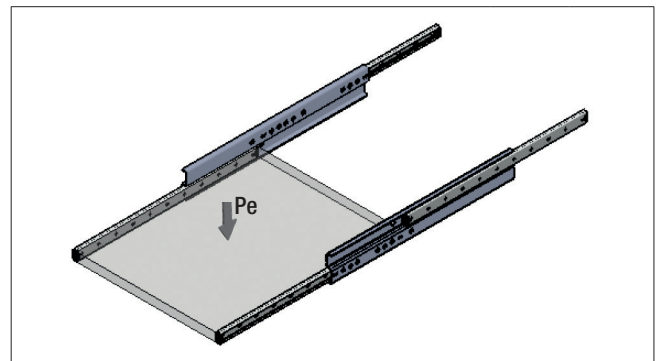


Fig.40

For telescopic rails TLQ...P the calculation might also include moments and axial load.

$$\left(\frac{Pe_{ax}}{C_{Oax}} + \frac{Pe_{rad}}{C_{Orad}} + \frac{Me_x}{M_x} + \frac{Me_y}{M_y} + \frac{Me_z}{M_z} \leq \frac{1}{S_0} \right)$$

Fig.39

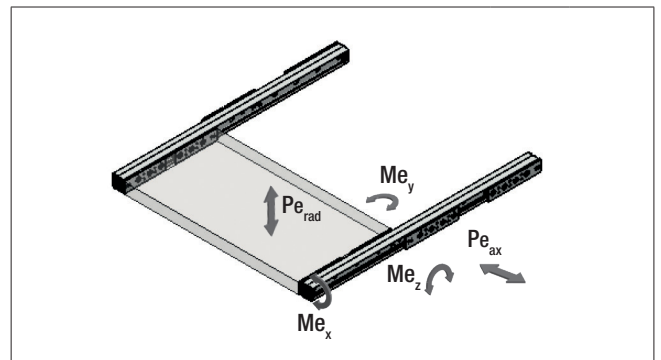


Fig.41

Where:

Pe_{rad} = applied radial load

Pe_{ax} = applied axial load

Me_x^* , Me_y , Me_z = applied moments

C_{Orad} = radial load capacity

C_{Oax} = axial load capacity

M_x , M_y , M_z = moment capacities

* Me_x moment exist only in case of use a single telescopic rail

If using a single telescopic rail, the values C_{Orad} , C_{Oax} , M_y and M_z in the formula Fig.39 must be divided by 2 (M_x is always and only referred to a single rail).

■ **Service life**

The service life is defined as the time span between commissioning and the first sign of fatigue or wear indications on the raceways. The service life of a telescopic rail is dependent on several factors, such as the effective load, the installation precision, occurring shocks and vibrations, the operating temperature, the ambient conditions and the lubrication.

Calculation of the service life is based exclusively on the loaded ball bearings. In practice, the decommissioning of the bearing, due to its destruction or extreme wear of a component, represents the end of service life.

This is taken into account by an application coefficient (fi in the formula below), so the service life consists of:

| | |
|---|--|
| $L_{cy} = 50 \cdot \left(\frac{C}{P_e} \cdot \frac{1}{f_i} \right)^3 \cdot \frac{1}{H} \cdot 10^6$ $L_{km} = 100 \cdot \left(\frac{C}{P_e} \cdot \frac{1}{f_i} \right)^3$ | <p>Lcy = calculated service life [num. of cycles] Lkm = calculated service life [Km] C = Dynamic load coefficient Pe = Equivalent load applied [N] H = Stroke [mm] fi = Application coefficient</p> |
|---|--|

Fig.42

Application coefficient fi

The correction factor fi applied to the theoretical calculation formula has the sole purpose of guiding the designer quantitatively on the influence in the lifetime estimation of the real application conditions without any pretense of precision. For more details please contact our technical department.

| Coefficient fi | Operating conditions |
|----------------|---|
| 1 - 1.5 | Correct load sizing, rigid structures, routine lubrication, clean ambient |
| 1.5 - 2 | Intermediate conditions |
| 2 - 3.5 | Approximative load sizing, unprecise non rigid structures, dusty not clear ambient. |

Tab.13

Equivalent load applied Pe

When the load P is not perfectly centered, the equivalent load Pe must be calculated as shown in Fig.43, otherwise, with the load perfectly centered:

$$P_e = P_{rad}$$

Fig.43

When using a pair of telescopic rails serie TLQ, in presence of simultaneous load P_{rad} , P_{ax} and moments M_y , M_z (M_x only in case of single rail) :

$$P_e = C_{o_{rad}} \cdot \left(\frac{P_{e_{rad}}}{C_{o_{rad}}} + \frac{P_{e_{ax}}}{C_{o_{ax}}} + \frac{M_{e_x}}{M_x} + \frac{M_{e_y}}{M_y} + \frac{M_{e_z}}{M_z} \right)$$

Fig.44

If using a single telescopic rail, the values $C_{o_{rad}}$, $C_{o_{ax}}$, M_y and M_z in the formula Fig.44 must be divided by 2 (M_x is always and only referred to a single rail).



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